

**Flow Rating Analysis for Pump Station S-332C  
IOP Emergency Pump Station, C-111 Basin**

*Technical Publication ERA # 449*



***Mark Wilsnack***

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**Stream Gauging, Engineering & Hydraulic Support Unit  
Operations & Hydro Data Management Division  
South Florida Water Management District**



## **Executive Summary**

A rating analysis of S-332C was carried out using the conventional case 8 model. The model equation was fit to the performance curve that depicts the TSH vs discharge relationship for each installed pump type. Flows computed with each equation agree with those obtained from its respective performance curve to within 0.2%. Furthermore, errors in computed flows resulting from uncertainties in computed head losses were estimated to be about 2% or less.

Despite these favorable results, it is recommended that the rating equations be compared with measured flows. Because of the hydraulic conditions at the downstream end of the discharge piping, it is suggested that an ADFM be used to monitor discharges. Furthermore, if feasible, it is recommended that head losses within the discharge piping be measured under a variety of discharges in order to evaluate pipe roughness under field conditions.

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## **Introduction**

Pump station S-332C is a component of Alternative 7R for the Interim Operational Plan (IOP) within the C-111 basin. Its functional purposes are similar to those of S-332B in that it transfers water from the C-111 borrow canal to a detention basin located within the eastern ENP. It is equipped with 5 vertical, axial-flow pumps manufactured by the MWI / Couch company and mounted on an outdoor platform. Four are driven by Caterpillar model 3406E diesel engines with a nominal design speed of 1800 RPM. The fifth is driven by an electric US Motors engine with a nominal speed of 1800 RPM. The discharge pipes for all pumps extend approximately one half a mile into the ENP and terminate at the associated detention reservoir.

## **Objectives and Scope**

The primary purpose of the rating analyses conducted in this study is to enable flows through S-332C to be estimated using measured head water elevations, tail water elevations and pump engine speeds. A secondary objective is to estimate the range of expected pipeline velocities in order to help ensure that the most appropriate flow measurement equipment is used. The hydraulic rating equations are based on pump performance characteristics, hydraulic properties of the pump station piping and appurtenances, and sound engineering principles. Since S-332C is relatively new and has not yet been acquired by the District, no flow measurements were available for calibrating the rating equations.

## **Station Design**

The diesel engine-driven pumps are of model number NW342x48 with an impeller diameter of 42 inches and a design speed of 404 RPM. The electric engine-driven pump is of model number NW330x48 with an impeller diameter of 30 inches and a design speed of 620 RPM. A conceptual cross section of a diesel engine-driven pump along with its discharge conduit is shown in figure 1. The corresponding cross section for the electric engine-driven pump is similar. Figure 2 provides detailed plan and profile views of the discharge piping that connects the pump station with the detention reservoir. Each pump discharges directly to about 60 feet of steel pipe that is connected at its downstream end to about one half mile of CMP. Each of these conduits terminates in a concrete outlet structure that is open to the reservoir (figure 3). Table 1 contains the relevant specifications of the station piping and appurtenances while figures 4 contain the pump performance curves. The Darcy-Weisbach friction factor values for the CMP were derived from the estimated range of Manning's n values shown in figure B-3 of HDS 5 (FHWA, 1985). Appendix A contains the associated calculations. These friction values appear to agree with those provided by FHWA (1980).

## **Rating Analysis**

The procedure implemented here for developing the rating curves reflects the standard procedure presented by Imru and Wang (2004). Previous applications of this procedure to other pump

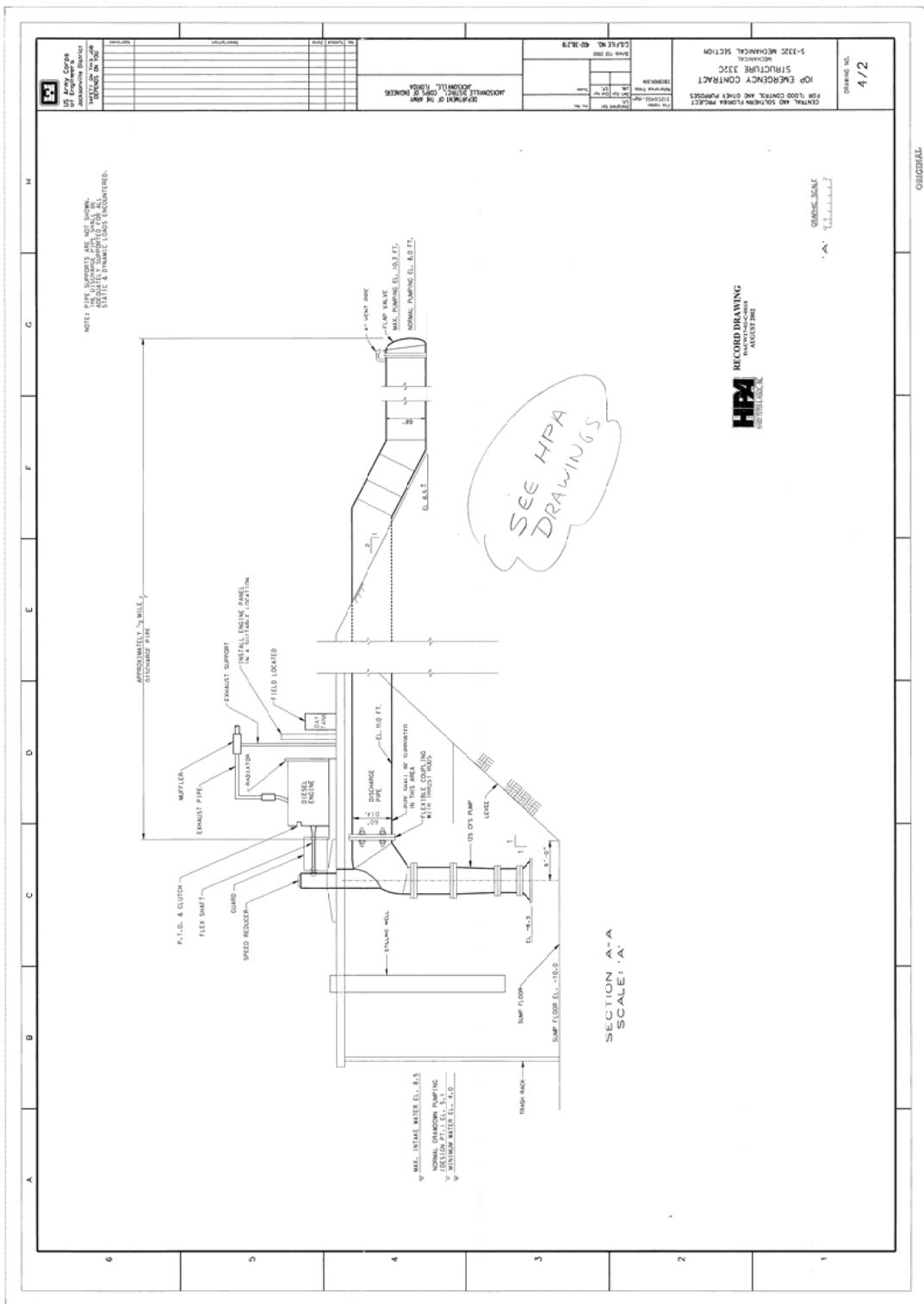


Figure 1. Conceptual cross section of S-332C pumps and discharge piping

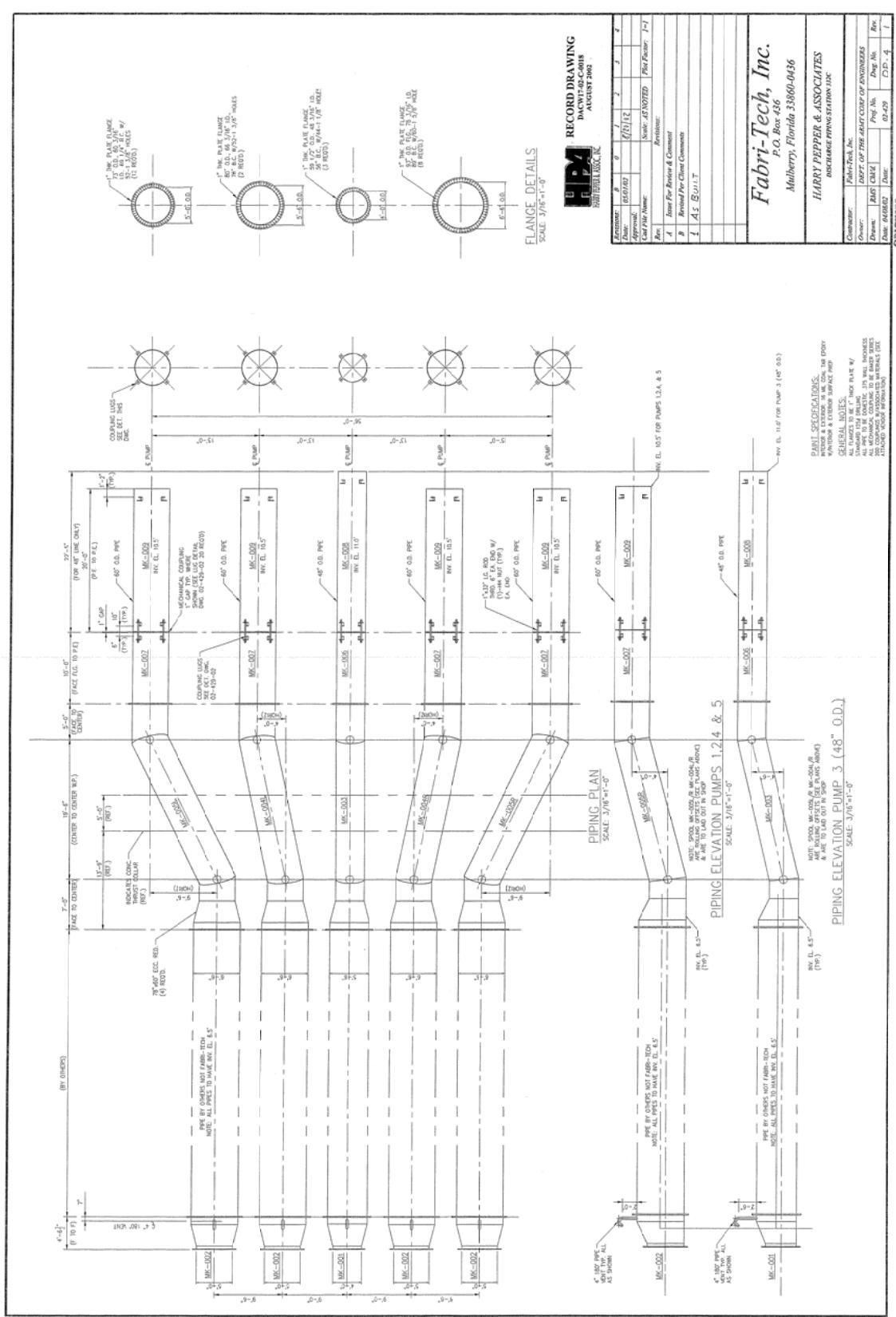
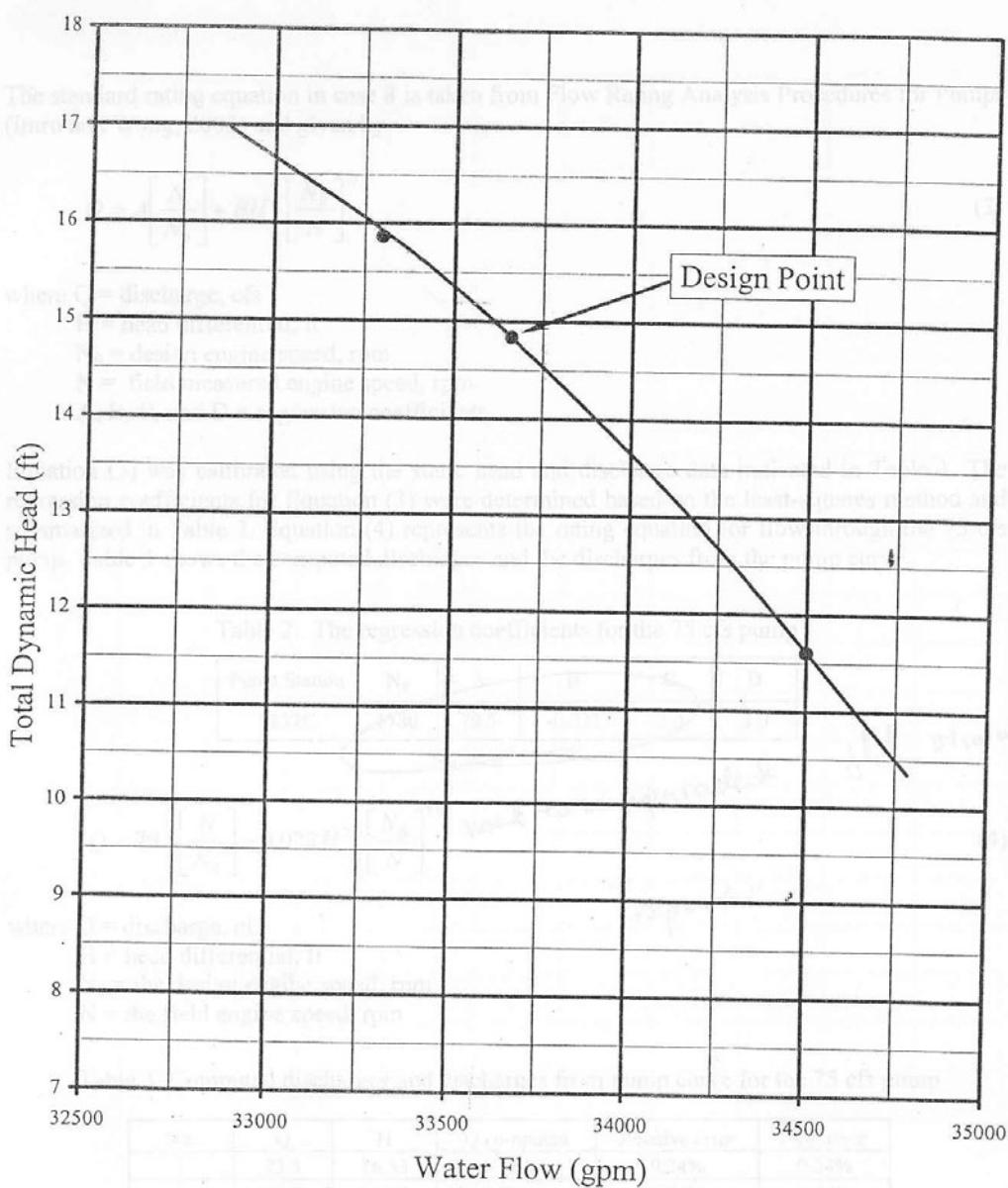


Figure 2. Plan and profile views of the discharge conduits



Figure 3. S-332C outlet structure at the detention reservoir



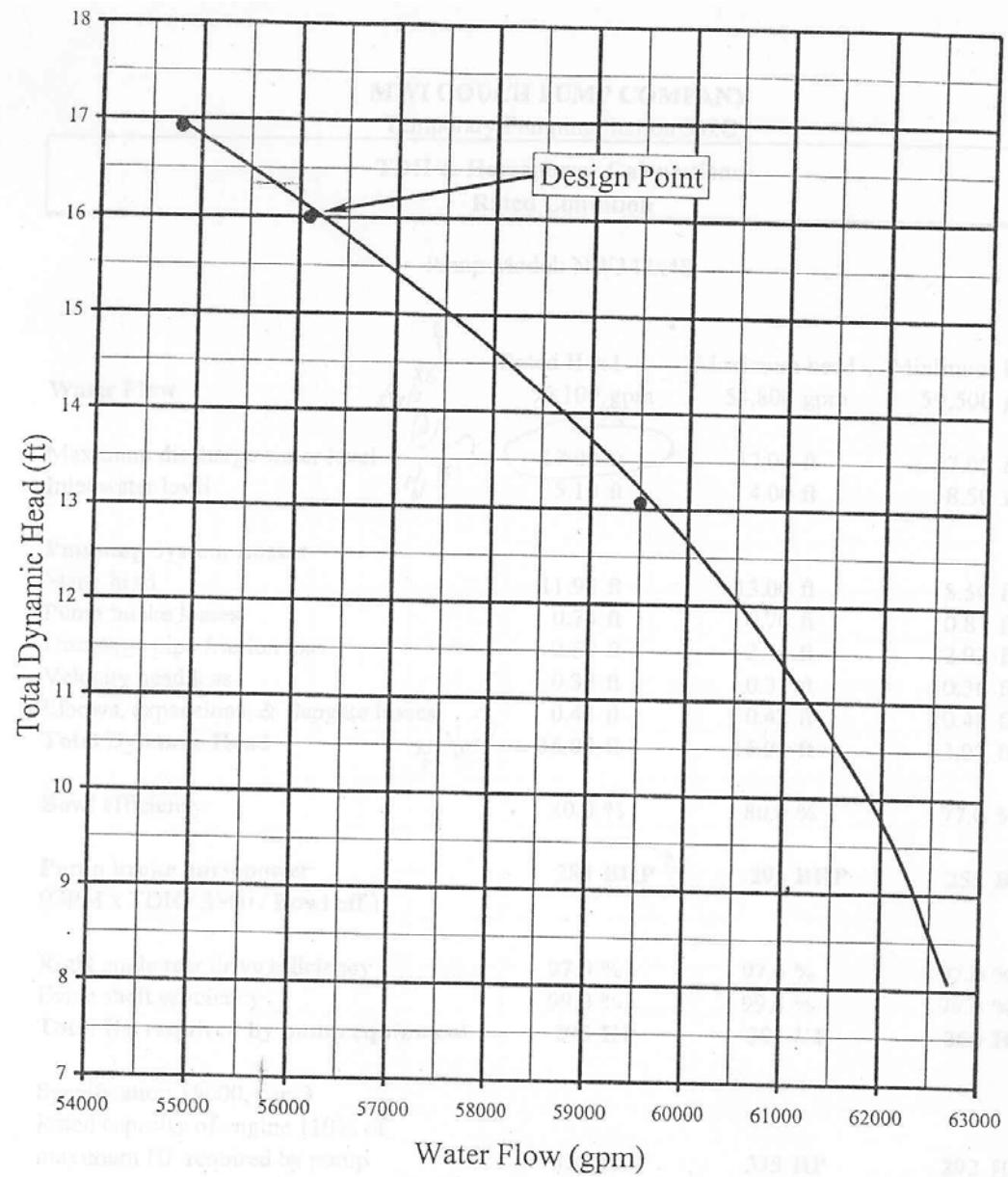
PUMP BOWL PERFORMANCE CURVE	
Project: US Army Corps S-332C	
TYPE: AXIAL FLOW	PROPELLER DIA: 30"
MODEL NO: NW330x48	SPEED: 620 RPM
INTAKE DIA: 45"	DISCHARGE DIA: 66"
Electric motor: 250 Hp @ 1780 rpm w/ beltdrive	
SINGLE STAGE PERFORMANCE FOR TWO STAGES MULTIPLY HEAD AND HORSEPOWER BY 2.0 AND EFFICIENCY BY 1.0 PERFORMANCE IS BASED ON PUMPING CLEAR, NON-AERATED WATER, WITH A SPECIFIC GRAVITY OF 1.0, TEMPERATURE 85 DEG F OR LESS AND AT SEA LEVEL. PUMP PERFORMANCE MAY BE AFFECTED BY HIGHER TEMPERATURES, SPECIFIC GRAVITY, ALTITUDES AND SUMP CONDITIONS.	

IT IS HEREBY CERTIFIED THAT THIS CURVE REPRESENTS THE TRUE PERFORMANCE CHARACTERISTICS OF THE MWI PUMP MODEL SHOWN AND WAS OBTAINED BY SCALE MODEL TEST AND CALCULATIONS IN ACCORDANCE WITH STANDARDS OF THE HYD...

MWI PUMP CORPORATION  
CERTIFICATE

MWI PUMP CORPORATION  
Deerfield Beach, Florida

Figure 4a. Pump performance curves for the electric motor-driven pump



PUMP BOWL PERFORMANCE CURVE	
Project: US Army Corps S-332C	
TYPE: AXIAL FLOW	PROPELLER DIA: 42"
MODEL NO: NW342x48	SPEED: 404 RPM
INTAKE DIA: 63"	DISCHARGE DIA: 78"
Diesel Engine: 425 Hp @ 1800 rpm w/ 9:2 gearhead	
SINGLE STAGE PERFORMANCE FOR TWO STAGES MULTIPLY HEAD AND HORSEPOWER BY 2.0 AND EFFICIENCY BY 1.0. PERFORMANCE IS BASED ON PUMPING CLEAR, NON-AERATED WATER, WITH A SPECIFIC GRAVITY OF 1.0, TEMPERATURE 85 DEG F OR LESS AND AT SEA LEVEL. PUMP PERFORMANCE MAY BE AFFECTED BY HIGHER TEMPERATURES, SPECIFIC GRAVITY, ALTITUDES AND SUMP CONDITIONS.	

IT IS HEREBY CERTIFIED THAT THIS CURVE REPRESENTS THE TRUE PERFORMANCE CHARACTERISTICS OF THE MWI PUMP MODEL SHOWN AND WAS OBTAINED BY SCALE MODEL TEST AND CALCULATIONS IN ACCORDANCE WITH STANDARDS OF THE HYDRAULIC INSTITUTE.

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CERTIFIED BY

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Deerfield Beach, Florida

Figure 4b. Pump performance curves for the diesel engine-driven pump

Table 1. Hydraulic properties of S-332C discharge piping

Pipe	Parameter	Diesel Pumps		Electric Pump		Source	
STEEL	length (ft)	62		62		record dwgs	
	O.D. (in)	60		48		record dwgs	
	wall thickn (in)	0.375		0.375		Sanks (1989)	
	I.D. (ft)	4.9375		3.9375		-----	
	Area (sqft)	19.15		12.18		-----	
	$\epsilon$ (min) (ft)	0.00015		0.00015		Hyd Inst (1990)	
	$\epsilon$ (max) (ft)	0.0006		0.0006		Sanks (1989), C=130	
	#	$K_{min}$	$K_{max}$	#	$K_{min}$	$K_{max}$	
25° miter bnd	2	0.066	0.154	0	0.066	0.154	Hyd Inst (1990)
12.5° miter bnd	2	0.042	0.062	2	0.042	0.062	Hyd Inst (1990)
enlgr @ us end	1	0.19	0.57	0	0	0	Hyd Inst (1990)
enlgr @ ds end	1	0.45	1.35	1	0.45	1.35	Hyd Inst (1990)
CMP	length (ft)	2050		2050		record dwgs	
	I.D. (ft)	6.5		5.5		record dwgs	
	Area (sqft)	33.18		23.76		-----	
	f(min)	0.052	(fully turbulent)	0.055	(fully turbulent)	HDS 5, fig B3; see calcs	
	f(max)	0.078	(fully turbulent)	0.082	(fully turbulent)		
	#	$K_{min}$	$K_{max}$	#	$K_{min}$	$K_{max}$	
reduc @ ds end	1	0.02	0.04	1	0.02	0.04	Sanks (1989)
exit	1	1	1	1	1	1	-----

station rating analyses are explained in detail by Wilsnack and Li (2006). The model rating equation applied to S-332C is the standard case 8 model:

$$Q = A \left( \frac{N}{N_o} \right)^C + BH^C \left( \frac{N_o}{N} \right)^{2C-1} \dots \dots \dots \quad (1)$$

Where Q is the discharge at a speed of N RPM, H is the TSH,  $N_o$  is the design engine or pump speed, and A, B and C are coefficients to be determined through regression. The form of this expression was determined through dimensional analysis and is based on the pump affinity laws. For pumps driven by electric motors,  $N_o = N$  so the ratios involving these parameters are eliminated.

As indicated previously, there are no discharge measurements available, so the objective was to fit equation (1) to the *pump station* performance curves (i.e. the static head versus discharge relationships). These were obtained as usual from the manufacturer's pump performance curves by subtracting the head losses associated with a given discharge rate from the corresponding value of TDH. The results are shown in figures 5. Several pump station performance curves were computed to evaluate the effects of uncertainties in the head loss calculations. The supporting calculations are provided in appendix B. Using the PROC NLIN procedure of SAS, equation (1) was fit to each of the curves in figures 5 depicting average head losses. The resultant coefficients

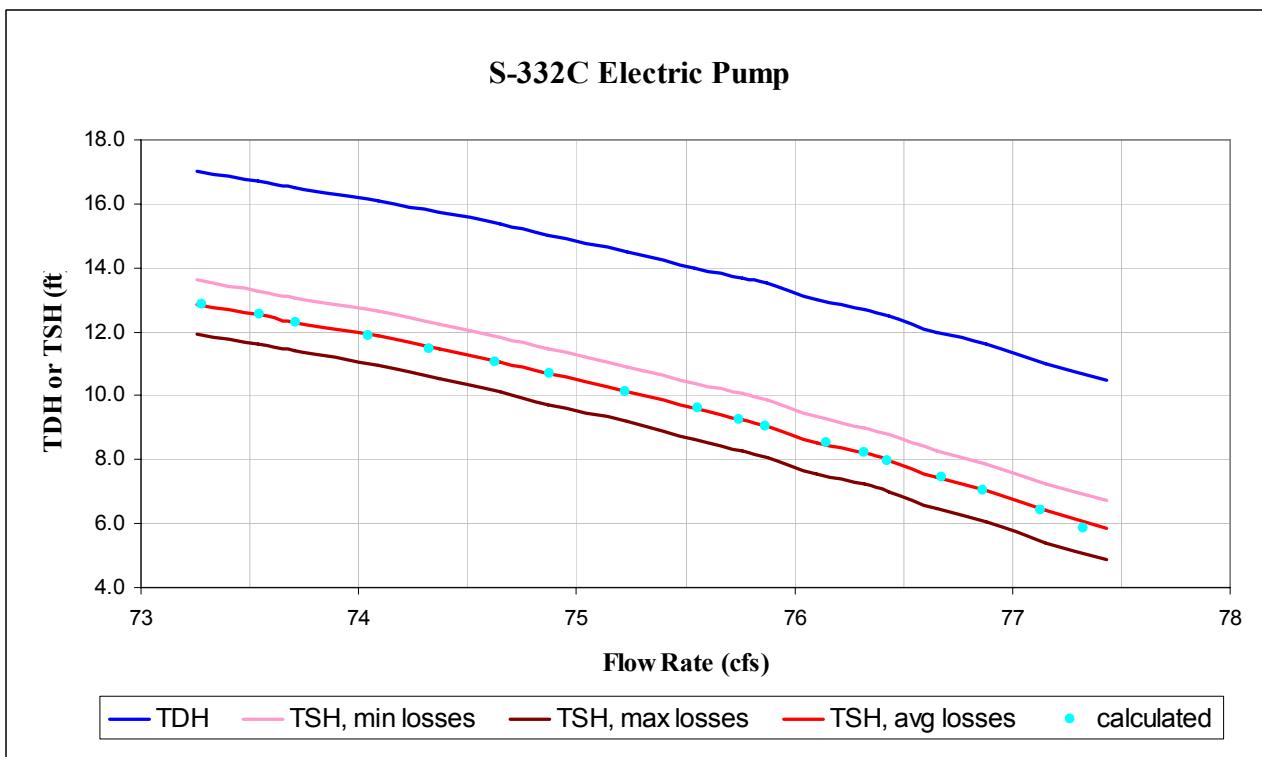


Figure 5a. Pump performance curves for the electric motor-driven pump

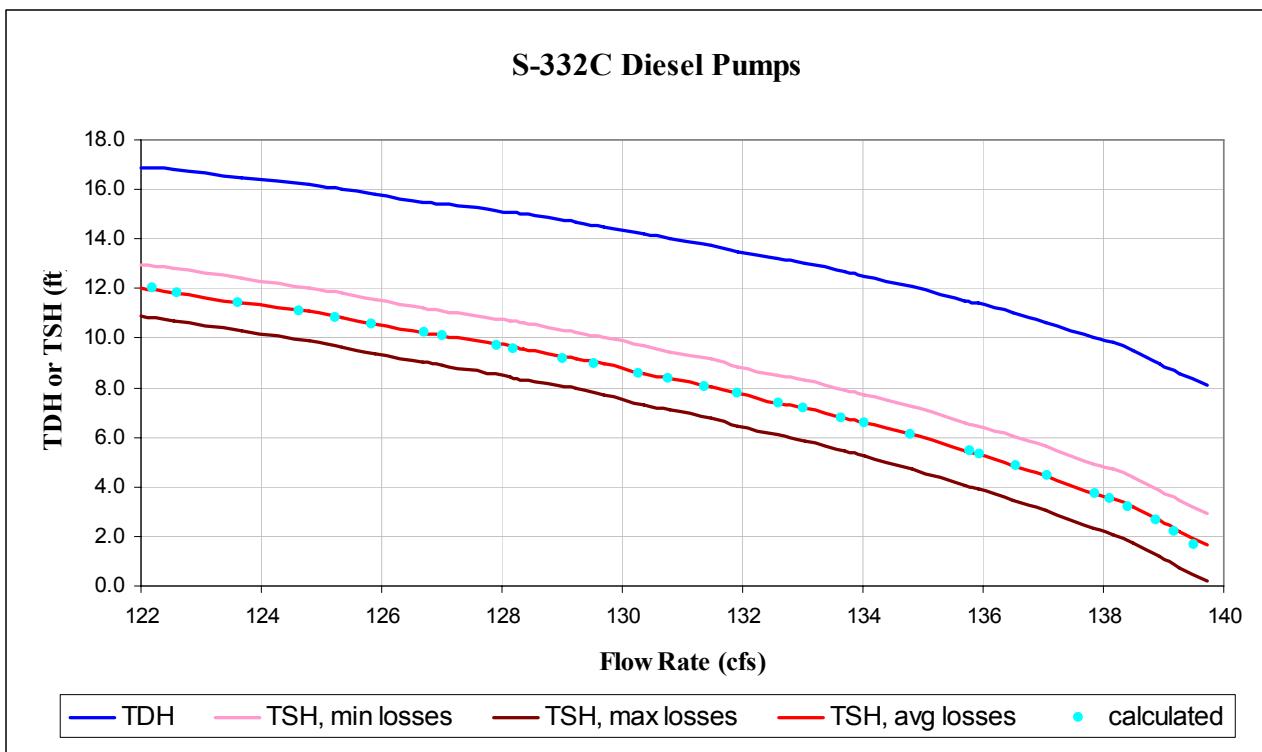


Figure 5b. Pump performance curves for the diesel engine-driven pump

are provided in table 2 while computed flow rates are shown in figures 5. It should also be noted that the pump station performance curves shown in figures 5 indicate that the uncertainty in flow rate due to uncertainties in computed head losses is less than about 2% of the flow rate.

Table 2. Values of the rating equation parameters for the S-332 pumps

Parameter		Electric Pump	Diesel Pump
<b>A</b>	<i>lower limit, approx. 95% C.I.</i>	78.177	139.9
	<i>estimated value</i>	78.380	140.0
	<i>upper limit, approx. 95% C.I.</i>	78.583	140.2
<b>B</b>	<i>lower limit, approx. 95% C.I.</i>	-0.0416	-0.213
	<i>estimated value</i>	-0.0298	-0.195
	<i>upper limit, approx. 95% C.I.</i>	-0.0179	-0.176
<b>C</b>	<i>lower limit, approx. 95% C.I.</i>	1.871	1.781
	<i>estimated value</i>	2.014	1.818
	<i>upper limit, approx. 95% C.I.</i>	2.156	1.855

### Discharge and Velocity Ranges

In order to estimate the expected range of operating conditions, system performance curves were computed for the expected minimum and maximum head losses and are plotted in figures 6.

Associated with these head losses are estimated minimum, average and maximum static heads of 1, 2.9 and 5.4 feet NGVD, respectively. These static heads were based on information provided in the record drawings and the Interim Operational Plan under storm conditions.

Within the estimated range of static heads, it is evident that discharges through the 78-inch CMP could range from about 134 cfs to somewhere around 140 cfs, although the upper limit cannot be accurately estimated due to the upper discharge limit of the pump performance curve. According to figure 6b, the diesel engine-driven pumps will most likely operate at a discharge rate of about 139 cfs. This is approximately 11% higher than the design discharge rate of 125 cfs. The corresponding velocity is 4.2 ft/s. Similarly, figure 6a suggests that discharges through the 66-inch CMP will be at least 77 cfs while the upper limit cannot be determined. Furthermore, the expected operating point for the electric engine-driven pump cannot be determined due to the upper discharge limit of the pump performance curve. Apparently, this pump will discharge at a rate somewhat greater the rated value of 75 cfs. Hence, the pump station operating characteristics shown in figures 6 indicate that the pumps will operate at points near the extreme right ends of their performance curves.

### Stream Gauging Data Needs

Given the absence of any discharge measurements, the flow data needs can be easily summarized as given in table 3 (Hua Li, personal communication). In order to obtain data over all the static head ranges shown, it is possible that some of the flow measurements will have to be obtained during designated pre or post storm conditions.

## Summary and Conclusions

A rating analysis of S-332C was carried out using the conventional case 8 model. The model equation was fit to the performance curve that depicts the TSH vs discharge relationship for each installed pump type. Flows computed with each equation agree with those obtained from its respective performance curve to within 0.2%. Furthermore, errors in computed flows resulting from uncertainties in computed head losses were estimated to be about 2% or less.

Despite these favorable results, it is recommended that the rating equations be compared with measured flows. Because of the hydraulic conditions at the downstream end of the discharge piping, it is suggested that an ADFM be used to monitor discharges.

Furthermore, if feasible, it is recommended that head losses within the discharge piping be measured under a variety of

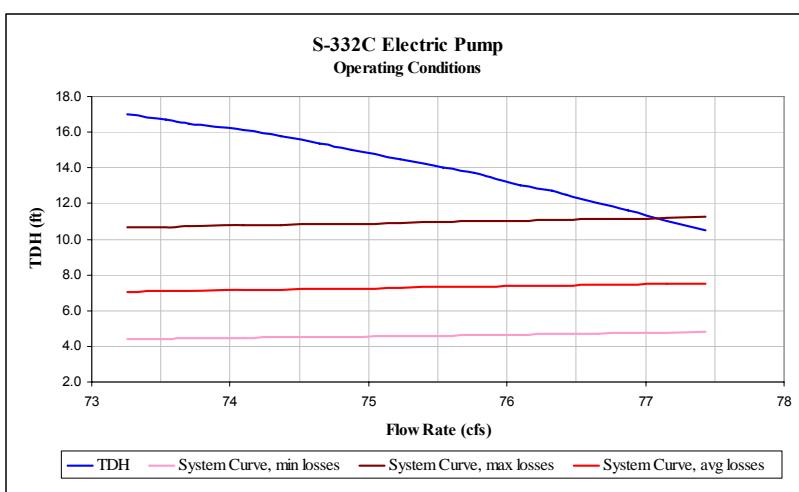


Figure 6a. Operating conditions for the electric motor-driven pump

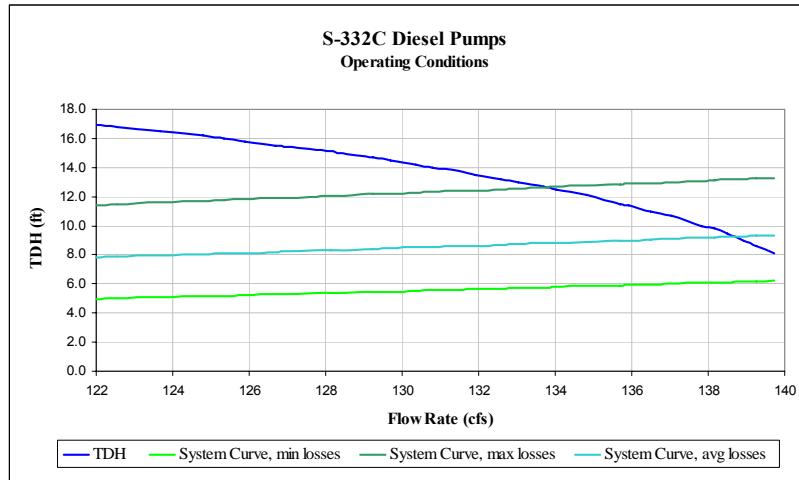


Figure 6b. Operating conditions for the diesel engine-driven pump  
discharges in order to evaluate pipe roughness under field conditions.

Table 3. Stream gauging needs for pump station S-332C.

Unit	TSH (ft)	RPM			
		900 - 1200	1200 - 1500	1500 - 1800	1800
Diesel (1,2,4,5)	0~4	5	5	5	
	4~8	5	5	5	
	8~12	5	5	5	
Electric (3)	0~3				5
	3~6				5
	6~9				5

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- Federal Highway Administration. 1980. *Hydraulic Flow Resistance Factors for Corrugated Metal Conduits*. Report No. FHWA-TS-80-216, US Department of Transportation, Federal Highway Administration, McLean, VA, 103 pp.
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- Imru, M. and Y. Wang. 2004. Flow Rating Development for New Pump Stations. Technical Publication EMA # 419, South Florida Water Management District, West Palm Beach, Florida, 44 pp.
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## **Appendix A. Estimation of Friction Factors for CMP**



South Florida Water Management District  
OPERATIONS & HYDRO DATA MANAGEMENT DIVISION

## Calculations

Form #0230  
Rev.11/97

Project: S-332 C RATING ANALYSIS Sheet No. 1 of 1  
Subject: ESTIMATE RANGE OF DARCY-WEISBACH f Job No. / Program Code: \_\_\_\_\_  
Engineer: WILSNACK Date: 3/26/07 Checked By: \_\_\_\_\_

$$S_{DW} = \left(\frac{f}{D}\right) \frac{V^2}{2g} \quad S_M = \frac{185.03}{D^{4/3}} n^2 \left(\frac{V^2}{2g}\right)$$

$$\frac{f}{D} \left(\frac{V^2}{2g}\right) = \frac{185.03}{D^{4/3}} n^2 \left(\frac{V^2}{2g}\right)$$

$$\boxed{f = 185.03 \frac{n^2}{D^{4/3}}}$$

FROM FIGURE B-3 OF HDS 5, THE EXPECTED RANGE  
OF  $n$  CAN BE TAKEN AS  $0.023 \leq n \leq 0.028$ .

THUS, CAN WRITE

	$n=0.023$	$n=0.028$
66" $\phi$	$f=0.055$	$f=0.082$
78" $\phi$	$f=0.052$	$f=0.078$

CHECK TYPE OF FLOW:

For  $Q \approx 75$  cfs THRU THE 66"  $\phi$  CMP,  $V = \frac{Q}{A}$   
 $= 3.16$  ft/s. For 125 cfs THRU THE 78"  $\phi$  CMP,  
 $V = 2.26$  ft/s. THESE RESULT IN NR VALUES OF  
 $1.5 - 2 ( \times 10^6 )$ . ACCORDING TO THE MOODY DIAGRAM,  
FLOW IS WHOLLY TURBULENT THRU A ROUGH PIPE, SO  
 $f$  CAN BE ASSUMED CONSTANT.

## **Appendix B. Head Loss Calculations**

Table Bla. Minimum head losses associated with the diesel engine-driven pumps

Pump Performance @ 404 RPM				Steel Pipe								Steel Pipe								CMP	
MDH (ft)	Q(gpm)	Q(cfs)	V(fts)	N <sub>R</sub>	V <sup>2</sup> /2g (ft)	Sources & Lam (1976)	f	h = f(L/D)V <sup>2</sup> /2g	h <sub>m</sub> = Σ KV <sup>2</sup> /2g	V(fts)	N <sub>R</sub>	V <sup>2</sup> /2g (ft)	Sources & Lam (1976)	f	h = f(L/D)V <sup>2</sup> /2g	h <sub>m</sub> = Σ KV <sup>2</sup> /2g	Total Head Loss (ft)	Static Head (ft)			
16.30	54750	122.00	6.37	3.51E+06	0.63	0.01091	0.09	0.22	3.68	2.39E+06	0.21	0.05200	3.44	0.22	3.97	12.93					
16.30	55000	122.56	6.40	3.16E+06	0.64	0.01091	0.09	0.22	3.69	2.40E+06	0.21	0.05200	3.47	0.22	4.01	12.79					
16.30	55500	123.67	6.46	3.19E+06	0.65	0.01090	0.09	0.23	3.73	2.42E+06	0.22	0.05200	3.54	0.23	4.08	12.42					
16.20	56000	124.20	6.52	3.22E+06	0.66	0.01089	0.09	0.23	3.76	2.44E+06	0.22	0.05200	3.60	0.23	4.15	12.05					
16.00	56250	125.34	6.55	3.23E+06	0.67	0.01089	0.09	0.23	3.78	2.46E+06	0.22	0.05200	3.63	0.23	4.19	11.81					
15.80	56500	125.90	6.58	3.25E+06	0.67	0.01089	0.09	0.23	3.79	2.47E+06	0.22	0.05200	3.67	0.24	4.23	11.57					
15.50	56850	126.68	6.62	3.27E+06	0.68	0.01088	0.09	0.24	3.82	2.48E+06	0.23	0.05200	3.71	0.24	4.28	11.22					
15.40	57000	127.02	6.63	3.28E+06	0.68	0.01088	0.09	0.24	3.83	2.49E+06	0.23	0.05200	3.73	0.24	4.30	11.10					
15.10	57500	128.13	6.69	3.30E+06	0.70	0.01087	0.10	0.24	3.86	2.51E+06	0.23	0.05200	3.80	0.24	4.38	10.72					
15.00	57600	128.35	6.70	3.31E+06	0.70	0.01087	0.10	0.24	3.87	2.51E+06	0.23	0.05200	3.81	0.25	4.39	10.61					
14.70	58000	129.24	6.75	3.33E+06	0.71	0.01086	0.10	0.25	3.89	2.52E+06	0.24	0.05200	3.86	0.25	4.46	10.24					
14.50	58200	129.69	6.77	3.34E+06	0.71	0.01086	0.10	0.25	3.91	2.54E+06	0.24	0.05200	3.89	0.25	4.49	10.01					
14.20	58500	130.36	6.81	3.36E+06	0.72	0.01086	0.10	0.25	3.93	2.55E+06	0.24	0.05200	3.93	0.25	4.53	9.67					
14.00	58700	130.80	6.83	3.37E+06	0.72	0.01085	0.10	0.25	3.94	2.56E+06	0.24	0.05200	3.96	0.26	4.56	9.44					
13.75	59000	131.47	6.87	3.39E+06	0.73	0.01085	0.10	0.26	3.96	2.58E+06	0.24	0.05200	4.00	0.26	4.61	9.14					
13.50	59200	131.92	6.89	3.40E+06	0.74	0.01085	0.10	0.26	3.98	2.58E+06	0.25	0.05200	4.02	0.26	4.64	8.86					
13.20	59500	132.59	6.92	3.42E+06	0.74	0.01084	0.10	0.26	4.00	2.60E+06	0.25	0.05200	4.07	0.26	4.69	8.51					
13.00	59700	133.03	6.95	3.43E+06	0.75	0.01084	0.10	0.26	4.01	2.61E+06	0.25	0.05200	4.09	0.26	4.72	8.28					
12.70	60000	133.70	6.98	3.45E+06	0.76	0.01083	0.10	0.26	4.03	2.62E+06	0.25	0.05200	4.13	0.27	4.77	7.93					
12.50	60150	134.03	7.00	3.46E+06	0.76	0.01083	0.10	0.27	4.04	2.63E+06	0.25	0.05200	4.15	0.27	4.79	7.71					
12.10	60500	134.81	7.04	3.48E+06	0.77	0.01083	0.10	0.27	4.06	2.64E+06	0.26	0.05200	4.20	0.27	4.85	7.25					
11.50	60900	135.79	7.09	3.50E+06	0.77	0.01082	0.11	0.27	4.09	2.66E+06	0.26	0.05200	4.26	0.27	4.91	6.59					
11.40	61000	135.93	7.10	3.51E+06	0.78	0.01082	0.11	0.27	4.10	2.66E+06	0.26	0.05200	4.27	0.28	4.93	6.47					
11.00	61250	136.49	7.13	3.52E+06	0.79	0.01082	0.11	0.28	4.11	2.67E+06	0.26	0.05200	4.31	0.28	4.97	6.03					
10.65	61500	137.04	7.16	3.53E+06	0.80	0.01081	0.11	0.28	4.13	2.68E+06	0.26	0.05200	4.34	0.28	5.01	5.64					
10.00	61850	137.82	7.20	3.55E+06	0.80	0.01081	0.11	0.28	4.15	2.70E+06	0.27	0.05200	4.39	0.28	5.07	4.93					
9.80	62000	138.16	7.22	3.56E+06	0.81	0.01081	0.11	0.28	4.16	2.71E+06	0.27	0.05200	4.41	0.28	5.09	4.71					
9.50	62150	138.49	7.23	3.57E+06	0.81	0.01080	0.11	0.28	4.17	2.71E+06	0.27	0.05200	4.44	0.29	5.12	4.38					
9.00	62350	138.94	7.26	3.58E+06	0.82	0.01080	0.11	0.29	4.19	2.72E+06	0.27	0.05200	4.46	0.29	5.15	3.85					
8.60	62500	139.27	7.27	3.59E+06	0.82	0.01080	0.11	0.29	4.20	2.73E+06	0.27	0.05200	4.49	0.29	5.17	3.43					
8.10	62700	139.72	7.30	3.60E+06	0.83	0.01080	0.11	0.29	4.21	2.74E+06	0.28	0.05200	4.51	0.29	5.21	2.89					

Table Blb. Minimum head losses associated with the electric engine-driven pumps

Pump Performance @ 620 RPM				Steel Pipe								Steel Pipe								CMP	
MDH (ft)	Q(gpm)	Q(cfs)	V(fts)	N <sub>R</sub>	V <sup>2</sup> /2g (ft)	Sources & Lam (1976)	f	h = f(L/D)V <sup>2</sup> /2g	h <sub>m</sub> = Σ KV <sup>2</sup> /2g	V(fts)	N <sub>R</sub>	V <sup>2</sup> /2g (ft)	Sources & Lam (1976)	f	h = f(L/D)V <sup>2</sup> /2g	h <sub>m</sub> = Σ KV <sup>2</sup> /2g	Total Head Loss (ft)	Static Head (ft)			
17.00	32875	73.26	6.02	2.37E+06	0.56	0.01141	0.10	0.11	3.08	1.70E+06	0.15	0.05500	3.03	0.16	3.39	13.61					
16.70	33000	73.54	6.04	2.38E+06	0.57	0.01140	0.10	0.11	3.10	1.70E+06	0.15	0.05500	3.05	0.16	3.42	13.28					
16.50	33075	73.70	6.05	2.38E+06	0.57	0.01140	0.10	0.11	3.10	1.71E+06	0.15	0.05500	3.06	0.16	3.43	13.07					
16.10	33250	74.09	6.08	2.40E+06	0.57	0.01140	0.10	0.11	3.12	1.72E+06	0.15	0.05500	3.10	0.16	3.47	12.63					
15.75	33375	74.37	6.11	2.40E+06	0.58	0.01139	0.10	0.11	3.13	1.72E+06	0.15	0.05500	3.12	0.16	3.50	12.25					
15.35	33500	74.65	6.13	2.41E+06	0.58	0.01139	0.10	0.11	3.14	1.73E+06	0.15	0.05500	3.14	0.16	3.52	11.83					
15.00	33600	74.87	6.15	2.42E+06	0.59	0.01139	0.11	0.11	3.15	1.73E+06	0.15	0.05500	3.16	0.17	3.54	11.46					
14.50	33760	75.23	6.18	2.43E+06	0.59	0.01138	0.11	0.11	3.17	1.74E+06	0.16	0.05500	3.19	0.17	3.58	10.92					
14.00	33900	75.54	6.20	2.44E+06	0.60	0.01138	0.11	0.11	3.18	1.75E+06	0.16	0.05500	3.22	0.17	3.61	10.39					
13.70	34000	75.76	6.22	2.45E+06	0.60	0.01137	0.11	0.11	3.19	1.75E+06	0.16	0.05500	3.24	0.17	3.63	10.07					
13.50	34050	75.87	6.23	2.45E+06	0.60	0.01137	0.11	0.12	3.19	1.76E+06	0.16	0.05500	3.25	0.17	3.64	9.86					
13.00	34150	76.10	6.25	2.46E+06	0.61	0.01137	0.11	0.12	3.20	1.76E+06	0.16	0.05500	3.27	0.17	3.66	9.34					
12.70	34250	76.32	6.27	2.47E+06	0.61	0.01137	0.11	0.12	3.21	1.77E+06	0.16	0.05500	3.28	0.17	3.68	9.02					
12.50	34300	76.43	6.28	2.47E+06	0.61	0.01137	0.11	0.12	3.22	1.77E+06	0.16	0.05500	3.29	0.17	3.69	8.81					
12.00	34400	76.65	6.30	2.48E+06	0.62	0.01136	0.11	0.12	3.23	1.77E+06	0.16	0.05500	3.31	0.17	3.71	8.29					
11.60	34500	76.88	6.31	2.49E+06	0.62	0.01136	0.11	0.12	3.24	1.78E+06	0.16	0.05500	3.33	0.17	3.74	7.86					
11.00	34625	77.16	6.34	2.49E+06	0.62	0.01136	0.11	0.12	3.25	1.79E+06	0.16	0.05500	3.36	0.18	3.76	7.24					
10.50	34750	77.43	6.36	2.50E+06	0.63	0.01135	0.11	0.12	3.26	1.79E+06	0.16	0.05500	3.38	0.18	3.79	6.71					

Table B2a. Maximum head losses associated with the diesel engine-driven pumps

Pump Performance @ 404 RPM				CWP							
TDH (ft)	Q(gpm)	Steel Pipe									
		Q(cfs)	V(ft/s)	Swanson & Jain(1976)		$h = f(LD)^{1/2}g$		$h_m = \Sigma KV^2/2g$		$V(fts)$	
				$f$							
16.90	54750	122.00	6.37	3.10E+06	0.63	0.01299	0.10	0.52	3.68	2.39E+06	0.21
16.80	55000	122.56	6.40	3.10E+06	0.64	0.01299	0.10	0.53	3.69	2.40E+06	0.21
16.50	55500	123.67	6.46	3.10E+06	0.65	0.01298	0.11	0.54	3.73	2.42E+06	0.22
16.20	56000	124.79	6.52	3.20E+06	0.66	0.01298	0.11	0.55	3.76	2.44E+06	0.22
16.00	56250	125.34	6.55	3.20E+06	0.67	0.01298	0.11	0.55	3.78	2.46E+06	0.22
15.80	56500	125.90	6.58	3.20E+06	0.67	0.01297	0.11	0.56	3.79	2.47E+06	0.22
15.50	56850	126.68	6.62	3.20E+06	0.68	0.01297	0.11	0.56	3.82	2.48E+06	0.23
15.40	57000	127.02	6.63	3.20E+06	0.68	0.01297	0.11	0.57	3.83	2.49E+06	0.23
15.10	57500	128.13	6.69	3.30E+06	0.70	0.01297	0.11	0.58	3.86	2.51E+06	0.23
15.00	57600	128.35	6.70	3.31E+06	0.70	0.01296	0.11	0.58	3.87	2.51E+06	0.23
14.70	58000	129.24	6.75	3.30E+06	0.71	0.01296	0.12	0.59	3.89	2.53E+06	0.24
14.50	58200	129.69	6.77	3.30E+06	0.71	0.01296	0.12	0.59	3.91	2.54E+06	0.24
14.20	58500	130.36	6.81	3.30E+06	0.72	0.01296	0.12	0.60	3.93	2.55E+06	0.24
14.00	58700	130.80	6.83	3.30E+06	0.72	0.01296	0.12	0.60	3.94	2.56E+06	0.24
13.75	59000	131.47	6.87	3.30E+06	0.73	0.01295	0.12	0.61	3.96	2.58E+06	0.24
13.50	59200	131.92	6.89	3.40E+06	0.74	0.01295	0.12	0.61	3.98	2.58E+06	0.25
13.20	59500	132.59	6.92	3.42E+06	0.74	0.01295	0.12	0.62	4.00	2.60E+06	0.25
13.00	59700	133.03	6.95	3.42E+06	0.75	0.01295	0.12	0.62	4.01	2.61E+06	0.25
12.70	60000	133.70	6.98	3.42E+06	0.76	0.01295	0.12	0.63	4.03	2.62E+06	0.25
12.50	60150	134.03	7.00	3.42E+06	0.76	0.01295	0.12	0.63	4.04	2.63E+06	0.25
12.10	60500	134.81	7.04	3.42E+06	0.77	0.01294	0.13	0.64	4.06	2.64E+06	0.26
11.50	60900	135.71	7.09	3.50E+06	0.78	0.01294	0.13	0.65	4.09	2.66E+06	0.26
11.40	61000	135.93	7.10	3.51E+06	0.78	0.01294	0.13	0.65	4.10	2.66E+06	0.26
11.00	61250	136.49	7.13	3.52E+06	0.79	0.01294	0.13	0.65	4.11	2.67E+06	0.26
10.65	61500	137.04	7.16	3.52E+06	0.80	0.01294	0.13	0.66	4.13	2.68E+06	0.26
10.00	61850	137.82	7.20	3.55E+06	0.80	0.01293	0.13	0.67	4.15	2.70E+06	0.27
9.80	62000	138.16	7.22	3.56E+06	0.81	0.01293	0.13	0.67	4.16	2.71E+06	0.27
9.50	62150	138.49	7.23	3.57E+06	0.81	0.01293	0.13	0.67	4.17	2.71E+06	0.27
9.00	62350	138.94	7.26	3.58E+06	0.82	0.01293	0.13	0.68	4.19	2.72E+06	0.27
8.60	62500	139.27	7.27	3.59E+06	0.82	0.01293	0.13	0.68	4.20	2.73E+06	0.27
8.10	62700	139.72	7.30	3.60E+06	0.83	0.01293	0.13	0.69	4.21	2.74E+06	0.28

Table B2b. Maximum head losses associated with the electric engine-driven pumps

Pump Performance @ 620 RPM				CWP							
TDH (ft)	Q(gpm)	Steel Pipe									
		Q(cfs)	V(ft/s)	Swanson & Jain(1976)		$h = f(LD)^{1/2}g$		$h_m = \Sigma KV^2/2g$		$V(fts)$	
				$f$							
17.00	32875	73.26	6.02	2.37E+06	0.56	0.01361	0.12	0.25	3.08	1.70E+06	0.15
16.70	33000	73.54	6.04	2.38E+06	0.57	0.01360	0.12	0.25	3.10	1.71E+06	0.15
16.50	33250	73.70	6.08	2.40E+06	0.57	0.01360	0.12	0.26	3.12	1.72E+06	0.15
16.10	33375	74.09	6.11	2.40E+06	0.58	0.01360	0.12	0.26	3.13	1.72E+06	0.15
15.75	33500	74.65	6.13	2.41E+06	0.58	0.01360	0.12	0.26	3.14	1.73E+06	0.15
15.35	33600	74.87	6.15	2.42E+06	0.59	0.01360	0.13	0.26	3.15	1.73E+06	0.15
14.50	33760	75.23	6.18	2.43E+06	0.59	0.01359	0.13	0.26	3.17	1.74E+06	0.16
14.00	33900	75.54	6.20	2.44E+06	0.60	0.01359	0.13	0.27	3.18	1.75E+06	0.16
13.70	34000	75.76	6.22	2.45E+06	0.60	0.01359	0.13	0.27	3.19	1.75E+06	0.16
13.50	34050	75.87	6.23	2.45E+06	0.60	0.01359	0.13	0.27	3.19	1.76E+06	0.16
13.00	34150	76.10	6.25	2.46E+06	0.61	0.01359	0.13	0.27	3.20	1.76E+06	0.16
12.70	34250	76.32	6.27	2.47E+06	0.61	0.01359	0.13	0.27	3.21	1.77E+06	0.16
12.50	34300	76.43	6.28	2.47E+06	0.61	0.01358	0.13	0.27	3.22	1.77E+06	0.16
12.00	34400	76.65	6.30	2.48E+06	0.62	0.01358	0.13	0.27	3.23	1.77E+06	0.16
11.60	34500	76.88	6.31	2.49E+06	0.62	0.01358	0.13	0.28	3.24	1.78E+06	0.16
11.00	34625	77.16	6.34	2.49E+06	0.62	0.01358	0.13	0.28	3.25	1.79E+06	0.16
10.50	34750	77.43	6.36	2.50E+06	0.63	0.01358	0.13	0.28	3.26	1.79E+06	0.16

Table B3a. Average head losses associated with the diesel engine-driven pumps

Pump Performance @ 404 RPM				Steel Pipe								CWP			
TDH (ft)	Q(gpm)	Q(cfs)	V(ft/s)	N <sub>R</sub>	V <sup>2</sup> /2g (ft)	Swanson & Jain(1976)	f	h = f(L/D)V <sup>2</sup> /2g	N <sub>R</sub>	V(ft/s)	N <sub>R</sub>	V <sup>2</sup> /2g (ft)	f	h = f(L/D)V <sup>2</sup> /2g	
16.90	54750	122.00	6.37	3.1E+06	0.63	0.01191	0.09	0.37	3.68	2.39E+06	0.21	0.06369	4.22	0.23	11.99
16.80	55000	122.56	6.40	3.1E+06	0.64	0.01190	0.10	0.37	3.69	2.40E+06	0.21	0.06369	4.25	0.23	11.95
16.50	55500	123.67	6.46	3.19E+06	0.65	0.01190	0.10	0.38	3.73	2.42E+06	0.22	0.06369	4.33	0.23	11.46
16.20	56000	124.79	6.52	3.23E+06	0.66	0.01189	0.10	0.39	3.76	2.44E+06	0.22	0.06369	4.41	0.24	11.06
16.00	56250	125.34	6.55	3.25E+06	0.67	0.01189	0.10	0.39	3.78	2.46E+06	0.22	0.06369	4.45	0.24	10.82
15.80	56500	125.90	6.58	3.25E+06	0.67	0.01188	0.10	0.40	3.79	2.47E+06	0.22	0.06369	4.49	0.24	10.57
15.50	56850	126.68	6.62	3.27E+06	0.68	0.01188	0.10	0.40	3.82	2.48E+06	0.23	0.06369	4.55	0.25	10.21
15.40	57000	127.02	6.63	3.28E+06	0.68	0.01188	0.10	0.40	3.83	2.49E+06	0.23	0.06369	4.57	0.25	10.08
15.10	57500	128.13	6.69	3.30E+06	0.70	0.01187	0.10	0.41	3.86	2.51E+06	0.23	0.06369	4.65	0.25	9.69
15.00	57600	128.35	6.70	3.31E+06	0.70	0.01187	0.10	0.41	3.87	2.51E+06	0.23	0.06369	4.67	0.25	9.57
14.70	58000	129.24	6.75	3.33E+06	0.71	0.01187	0.11	0.42	3.89	2.53E+06	0.24	0.06369	4.73	0.26	9.19
14.50	58200	129.69	6.77	3.34E+06	0.71	0.01186	0.11	0.42	3.91	2.54E+06	0.24	0.06369	4.76	0.26	8.95
14.20	58500	130.36	6.81	3.36E+06	0.72	0.01186	0.11	0.42	3.93	2.55E+06	0.24	0.06369	4.81	0.26	8.60
14.00	58700	130.80	6.83	3.37E+06	0.72	0.01186	0.11	0.43	3.94	2.56E+06	0.24	0.06369	4.85	0.26	8.36
13.75	59000	131.47	6.87	3.39E+06	0.73	0.01185	0.11	0.43	3.96	2.58E+06	0.24	0.06369	4.90	0.26	8.05
13.50	59200	131.92	6.89	3.40E+06	0.74	0.01185	0.11	0.43	3.98	2.58E+06	0.25	0.06369	4.93	0.27	7.74
13.20	59500	132.59	6.92	3.42E+06	0.74	0.01185	0.11	0.44	4.00	2.60E+06	0.25	0.06369	4.98	0.27	7.40
13.00	59700	133.03	6.95	3.43E+06	0.75	0.01185	0.11	0.44	4.01	2.61E+06	0.25	0.06369	5.01	0.27	7.84
12.70	60000	133.70	6.98	3.44E+06	0.76	0.01184	0.11	0.45	4.03	2.62E+06	0.25	0.06369	5.06	0.27	5.90
12.50	60150	134.03	7.00	3.46E+06	0.76	0.01184	0.11	0.45	4.04	2.63E+06	0.25	0.06369	5.09	0.28	6.57
12.10	60500	134.81	7.04	3.48E+06	0.77	0.01184	0.11	0.45	4.06	2.64E+06	0.26	0.06369	5.15	0.28	6.11
11.50	60900	135.71	7.09	3.50E+06	0.78	0.01183	0.12	0.46	4.09	2.66E+06	0.26	0.06369	5.22	0.28	5.43
11.40	61000	135.93	7.10	3.51E+06	0.78	0.01183	0.12	0.46	4.10	2.66E+06	0.26	0.06369	5.23	0.28	6.09
11.00	61250	136.49	7.13	3.52E+06	0.79	0.01183	0.12	0.46	4.11	2.67E+06	0.26	0.06369	5.28	0.29	6.14
10.65	61500	137.04	7.16	3.53E+06	0.80	0.01183	0.12	0.47	4.13	2.68E+06	0.26	0.06369	5.32	0.29	6.19
10.00	61850	137.82	7.20	3.55E+06	0.80	0.01182	0.12	0.47	4.15	2.70E+06	0.27	0.06369	5.38	0.29	5.74
9.80	62000	138.16	7.22	3.56E+06	0.81	0.01182	0.12	0.48	4.16	2.71E+06	0.27	0.06369	5.41	0.29	5.30
9.50	62150	138.49	7.23	3.57E+06	0.81	0.01182	0.12	0.48	4.17	2.71E+06	0.27	0.06369	5.43	0.29	5.33
9.00	62350	138.94	7.26	3.58E+06	0.82	0.01182	0.12	0.48	4.19	2.72E+06	0.27	0.06369	5.47	0.30	6.37
8.60	62500	139.27	7.27	3.59E+06	0.82	0.01182	0.12	0.48	4.20	2.73E+06	0.27	0.06369	5.49	0.30	2.20
8.10	62700	139.72	7.30	3.60E+06	0.83	0.01181	0.12	0.49	4.21	2.74E+06	0.28	0.06369	5.53	0.30	6.44

Table B3b. Average head losses associated with the electric engine-driven pumps

Pump Performance @ 620 RPM				Steel Pipe								CWP			
TDH (ft)	Q(gpm)	Q(cfs)	V(ft/s)	N <sub>R</sub>	V <sup>2</sup> /2g (ft)	Swanson & Jain(1976)	f	h = f(L/D)V <sup>2</sup> /2g	N <sub>R</sub>	V(ft/s)	N <sub>R</sub>	V <sup>2</sup> /2g (ft)	f	h = f(L/D)V <sup>2</sup> /2g	
17.00	32875	73.26	6.02	2.37E+06	0.56	0.01246	0.11	0.18	3.08	1.70E+06	0.15	0.06716	3.70	0.16	4.15
16.70	33000	73.54	6.04	2.38E+06	0.57	0.01245	0.11	0.18	3.10	1.71E+06	0.15	0.06716	3.72	0.16	4.18
16.50	33075	73.70	6.05	2.38E+06	0.57	0.01245	0.11	0.18	3.12	1.72E+06	0.15	0.06716	3.74	0.17	4.20
16.10	33250	74.09	6.08	2.40E+06	0.57	0.01245	0.11	0.18	3.13	1.73E+06	0.15	0.06716	3.78	0.17	4.24
15.75	33375	74.37	6.11	2.40E+06	0.58	0.01244	0.11	0.19	3.14	1.73E+06	0.15	0.06716	3.81	0.17	4.27
15.35	33500	74.65	6.13	2.41E+06	0.58	0.01244	0.12	0.19	3.15	1.73E+06	0.15	0.06716	3.84	0.17	4.31
15.00	33600	74.87	6.15	2.42E+06	0.59	0.01244	0.12	0.19	3.17	1.74E+06	0.16	0.06716	3.86	0.17	4.33
14.50	33760	75.23	6.18	2.43E+06	0.59	0.01244	0.12	0.19	3.17	1.74E+06	0.16	0.06716	3.90	0.17	4.37
14.00	33900	75.54	6.20	2.44E+06	0.60	0.01243	0.12	0.19	3.18	1.75E+06	0.16	0.06716	3.93	0.17	4.41
13.70	34000	75.76	6.22	2.45E+06	0.60	0.01243	0.12	0.19	3.19	1.75E+06	0.16	0.06716	3.95	0.17	4.44
13.50	34050	75.87	6.23	2.45E+06	0.60	0.01243	0.12	0.19	3.19	1.76E+06	0.16	0.06716	3.96	0.18	4.45
13.00	34150	76.10	6.25	2.46E+06	0.61	0.01243	0.12	0.19	3.20	1.76E+06	0.16	0.06716	3.99	0.18	4.48
12.70	34250	76.32	6.27	2.47E+06	0.61	0.01243	0.12	0.19	3.21	1.77E+06	0.16	0.06716	4.01	0.18	4.50
12.50	34300	76.43	6.28	2.47E+06	0.61	0.01243	0.12	0.19	3.22	1.77E+06	0.16	0.06716	4.02	0.18	4.51
12.00	34400	76.65	6.30	2.48E+06	0.62	0.01242	0.12	0.20	3.23	1.78E+06	0.16	0.06716	4.05	0.18	4.54
11.60	34500	76.88	6.31	2.49E+06	0.62	0.01242	0.12	0.20	3.24	1.78E+06	0.16	0.06716	4.07	0.18	4.57
11.00	34625	77.16	6.34	2.49E+06	0.62	0.01242	0.12	0.20	3.25	1.79E+06	0.16	0.06716	4.10	0.18	4.60
10.50	34750	77.43	6.36	2.50E+06	0.63	0.01242	0.12	0.20	3.26	1.79E+06	0.16	0.06716	4.13	0.18	4.63